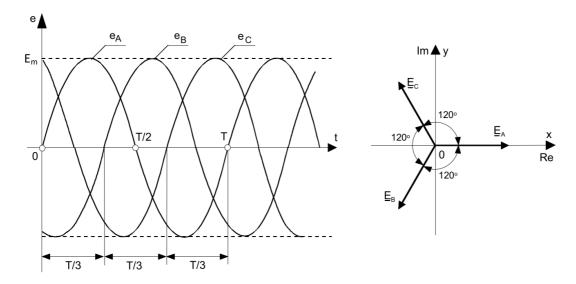
ELECTRICAL CIRCUITS 2 - CLASS 6 (16.04.2024)

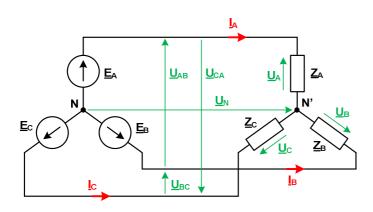
Three-phase circuits

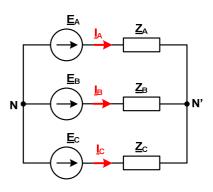
• Generator voltages (positive phase sequence):

$$\begin{array}{lll} e_{\scriptscriptstyle A}(t) = E_{\scriptscriptstyle m} \sin(\omega t) & \underline{E}_{\scriptscriptstyle A} = E e^{j0^\circ} \\ e_{\scriptscriptstyle B}(t) = E_{\scriptscriptstyle m} \sin(\omega t - 120^\circ) & \underline{E}_{\scriptscriptstyle B} = E e^{-j120^\circ} & \underline{E}_{\scriptscriptstyle A} + \underline{E}_{\scriptscriptstyle B} + \underline{E}_{\scriptscriptstyle C} = 0 \\ e_{\scriptscriptstyle C}(t) = E_{\scriptscriptstyle m} \sin(\omega t + 120^\circ) & \underline{E}_{\scriptscriptstyle C} = E e^{j120^\circ} & \underline{E}_{\scriptscriptstyle A} + \underline{E}_{\scriptscriptstyle B} + \underline{E}_{\scriptscriptstyle C} = 0 \\ \end{array} \qquad \begin{array}{ll} E_{\scriptscriptstyle m} & \text{- the peak (maximum) value} \\ \underline{E} & \text{- the complex value (phasor)} \\ E & \text{- the rms (effective) value} \end{array}$$



Balanced Wye-Wye (Y-Y) connection, three-wire system





Symbols in the circuit:

 $\underline{E}_A, \ \underline{E}_B, \ \underline{E}_C$ - phase voltages of the generator $\underline{I}_A, \ \underline{I}_B, \ \underline{I}_C$ - the line currents $\underline{U}_A, \ \underline{U}_B, \ \underline{U}_C$ - phase voltages of the load $\underline{Z}_A, \ \underline{Z}_B, \ \underline{Z}_C$ - the load impedances $\underline{U}_{AB}, \ \underline{U}_{BC}, \ \underline{U}_{CA}$ - line voltages (line-to-line) N - neutral point of the source \underline{U}_N - voltage between N and N' points N' - neutral point of the load

Balanced load:

$$\underline{Z}_A = \underline{Z}_B = \underline{Z}_C = \underline{Z}$$

• <u>*U*</u>_N voltage:

$$\underline{U}_{N} = \frac{\underline{E}_{A} \cdot \underline{Y}_{A} + \underline{E}_{B} \cdot \underline{Y}_{B} + \underline{E}_{C} \cdot \underline{Y}_{C}}{Y_{A} + Y_{B} + Y_{C}} \qquad \text{where:} \qquad \underline{Y}_{A} = \frac{1}{Z_{A}}, \quad \underline{Y}_{B} = \frac{1}{Z_{B}}, \quad \underline{Y}_{C} = \frac{1}{Z_{C}}$$

$$\underline{U}_A = \underline{E}_A$$
, $\underline{U}_B = \underline{E}_B$, $\underline{U}_C = \underline{E}_C$ because in the system with the balanced load: $\underline{U}_N = 0$

• The line currents:

$$\underline{I}_A = \frac{\underline{E}_A}{\underline{Z}_A}, \quad \underline{I}_B = \frac{\underline{E}_B}{\underline{Z}_B}, \quad \underline{I}_C = \frac{\underline{E}_C}{\underline{Z}_C}$$

the complex values (phasors): $\underline{I}_A + \underline{I}_B + \underline{I}_C = 0$

the rms (effective) values: $I_A = I_B = I_C$

• The line voltages (line-to-line):

$$\underline{U}_{AB} = \underline{E}_A - \underline{E}_B = \sqrt{3}Ee^{j30^{\circ}}$$

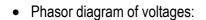
$$\underline{U}_{BC} = \underline{E}_B - \underline{E}_C = \sqrt{3}Ee^{-j90^{\circ}}$$

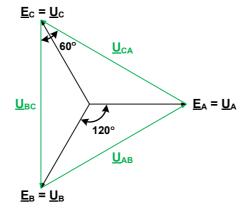
$$\underline{U}_{CA} = \underline{E}_C - \underline{E}_A = \sqrt{3}Ee^{j150^{\circ}}$$

the complex values (phasors): $\underline{U}_{AB} + \underline{U}_{BC} + \underline{U}_{CA} = 0$

Complex power:

the rms (effective) values: $U_{AB} = U_{BC} = U_{CA}$





• Active, reactive and apparent power:

$$P = U_A \cdot I_A \cdot \cos \varphi_A + U_B \cdot I_B \cdot \cos \varphi_B + U_C \cdot I_C \cdot \cos \varphi_C$$

$$Q = U_A \cdot I_A \cdot \sin \varphi_A + U_B \cdot I_B \cdot \sin \varphi_B + U_C \cdot I_C \cdot \sin \varphi_C$$

$$S = U_A \cdot I_A + U_B \cdot I_B + U_C \cdot I_C$$

$$S = U_A \cdot I_A + U_B \cdot I_B + U_C \cdot I_C$$

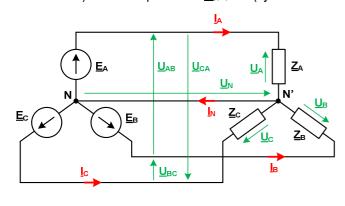
$$P = \text{Re}\{\underline{S}\}, \quad Q = \text{Im}\{\underline{S}\}, \quad S = \|\underline{S}\|$$

in the case of balanced load:

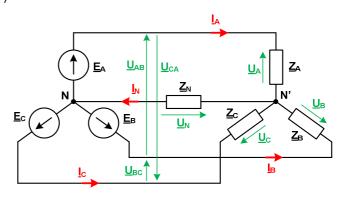
$$U_{\scriptscriptstyle A} = U_{\scriptscriptstyle B} = U_{\scriptscriptstyle C} = U_{\scriptscriptstyle ph}, \qquad I_{\scriptscriptstyle A} = I_{\scriptscriptstyle B} = I_{\scriptscriptstyle C} = I_{\scriptscriptstyle ph}, \qquad \cos \varphi_{\scriptscriptstyle A} = \cos \varphi_{\scriptscriptstyle B} = \cos \varphi_{\scriptscriptstyle C} = \cos \varphi_{\scriptscriptstyle ph}$$
 then:

$$P = 3 \cdot U_{ph} \cdot I_{ph} \cdot \cos \varphi_{ph}, \qquad Q = 3 \cdot U_{ph} \cdot I_{ph} \cdot \sin \varphi_{ph}, \qquad S = 3 \cdot U_{ph} \cdot I_{ph}$$

<u>Note</u>: all of the above relationships are also valid for four-wire balanced system with impedance $\underline{Z}_N = O$ (system on the left) or with impedance $\underline{Z}_N \neq O$ (system on the right).



$$\underline{U}_N = 0$$
, $\underline{I}_N = 0$

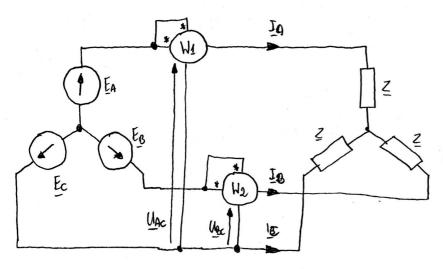


$$\underline{U}_N = 0$$
, $\underline{I}_N = 0$

ELECTRICAL CIRCUITS 2 - CLASS NO. 6 (16.04.2024)

PROBLEM #1

In a 3-phose balanced 1/4 system, the source voltage is Ephase = 230 V rms. The impedance per phase is Z=(8+j6)ul. Check whether an overcurrent circuit breaker with a rated current of 10A is sufficient to protect this circuit. Also, find the active power of the load and the readings of the watmeters.



$$E_{A} = 230e^{j00} = 230 \text{ V}$$
 $E_{B} = 230e^{j1200} = (-115-j189.19) \text{ V}$
 $E_{C} = 230e^{j1200} = (-115+j189.19) \text{ V}$

$$I_A = \frac{E_A}{2} = \frac{230}{8+j6} = (18.4-j13.8)A = 23e^{j36.87}A$$

$$I_8 = \frac{E_8}{2} = \frac{-115 - j \, 139.19}{8 + j6} = (21.15 - j \, 9.03) A = 23e^{-j.156.87}$$

Method 1

$$|I_A| = 23 A > 10 A$$
 $I_C = \frac{E_C}{Z} = \frac{-115 + j 199.19}{84.6} = (2.75 + j 22.83) A = 23e^{j83.13} A$

Method 2

$$S = E_{A} \cdot I_{A}^{*} + E_{B} \cdot I_{B}^{*} + E_{C} \cdot I_{C}^{*} = 230 \cdot (18.4 + j \cdot 13.8) + (-145 - j \cdot 199.49) \cdot (-24.45 + j \cdot 9.03) + (-145 + j \cdot 188.18) \cdot (2.75 - j \cdot 22.88)$$

$$P_{lood} = 12.686 \text{ L}$$

$$= 4232 + j \cdot 3474 + 4232 + j \cdot 3474 + 4232 + j \cdot 3474 = 12.686 + j \cdot 9522 \text{ VA}$$

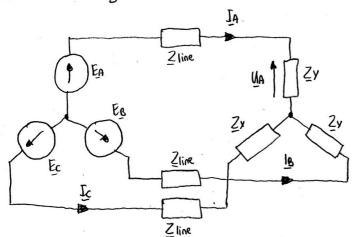
$$P_{lood}$$

Method 3

$$S_1 = U_{AC} \cdot I_A^* = (345 - j.188.18) \cdot (18.4 + j.13.8) = (9086.76 + j.1085.88) VA $\Rightarrow \rho_{WL} = 9086.76 W$$$

PROBLEM #2

In a 3-phase balanced V-V system, the source voltage is Ephase = $230 \,\text{V}$ ms. The impedance per phase is $2y = (8+9) \,\text{UL}$ and the line impedance per phase is $(0.5+j\,0.4) \,\text{UL}$. What should be the rated current of the overcurrent circuit breakers protecting the circuit? Standard rated currents are: 64, 404, 4



$$E_{A} = 230e^{j0^{\circ}} = 230 \text{ V}$$

$$E_{B} = 230e^{-j120^{\circ}} = (-115 - j \cdot 198.18) \text{ V}$$

$$E_{C} = 230e^{j120^{\circ}} = (-115 + j \cdot 198.18) \text{ V}$$

$$I_{A} = \frac{E_{A}}{Z_{x} + 2line} = \frac{230}{9 + j \cdot 18 + 0.5 + j \cdot 0.4} = \frac{230}{9.5 + j \cdot 18.4} = (12.23 - j \cdot 12.10) A = 17.21e^{-j \cdot 14.7} A$$

$$|I_{A}| = |I_{B}| = |I_{C}| = 17.21A$$

The rated current of the overcurrent circuit breaker should be: [20A]

The active power losses in the power line:

Zline = Rline + j Xline =
$$(0.5+j 0.4)VL$$

Plosses = 3 · Rline · I_{line}^2 = 3 · 0.5 · 19.21 = 3 · 148.09 = $[444.27 \ \text{W}]$

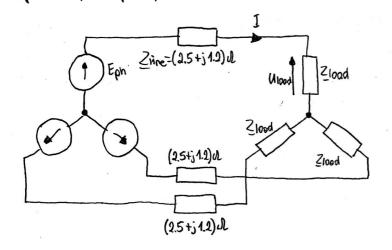
The percentage voltage drap:

$$\frac{\text{UA} = I_{A} \cdot 2y = (12.23 - j \cdot 12.40) \cdot (9 + j \cdot 9) = (218.04 + j \cdot 1.16) V = 218.04 e^{j0.3^{\circ}} V}{|U_{A}| = 218.04V |E_{A}| = 230 V}$$

$$\Delta U_{90} = \frac{|E_{A}| - |U_{A}|}{|E_{A}|} \cdot 10090 = \frac{230 - 218.04}{230} \cdot 10090 = [4.76590]$$

PROBLEM #3

In the 3-phase balanced Y-Y system, the load voltage is $Uload = 400 \angle -20^{\circ} \text{ V rms}$, the line impedance is (2.5+j.1.1)U, and the source voltage is Ephase = 440 V rms. Find the load impedance, its power, and the value of supplying current.



$$I = \frac{Eph}{Zline+Zlood}$$

$$I = \frac{Ulood}{Zlood}$$

$$Eph \cdot Zlood = Ulood (Zline + Zlood)$$

$$Zlood (Eph - Ulood) = Zline Ulood$$

$$Zlood = Zline \frac{Ulood}{Eph - Ulood}$$

$$\begin{array}{ll} \text{Uload} = 400 \, \mathrm{e}^{-\mathrm{j}20^{\circ}} = (375.88 \, -\mathrm{j} \, 136.81) \, \mathrm{V} \\ \text{Eph} = 440 \, \mathrm{e}^{\mathrm{j}80^{\circ}} = 440 \, \mathrm{V} \\ \text{Z line} = (2.5 \, +\mathrm{j} \, 1.2) \, \mathrm{N} \end{array}$$

$$\begin{array}{ll} \text{Zload} = \left(2.5 \, +\mathrm{j} \, 1.2\right) \cdot \frac{375.88 \, -\mathrm{j} \, 136.81}{440 \, -375.88 \, +\mathrm{j} \, 136.81} = \left[\left(3.9541 \, -\mathrm{j} \, 6.3081\right) \, \mathrm{N} \right] \end{array}$$

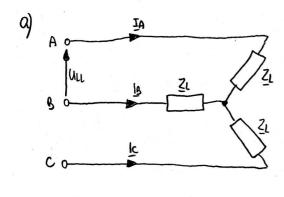
$$Iload = \frac{Uload}{2load} = \frac{400e^{-j20^{\circ}}}{3.7541 - j6.3081} = (42.1947 + j34.4698)A = [54.48e^{j39.2^{\circ}}A]$$

Pload = 3 · Re { Slood} = 3 · Re { Yrood · Irood } = 3 · Re { (375.88 - j 136.81) (42.1849 - j 34.4698)} = 3 · Re { (11144 - j 18728) = 3 · 11144 = 33433 W

PROBLEM #4

The line-to-line voltage of a balanced 3-phase distribution line is Uu = 380 V rms. The load impedance per phase is $Z_L = (30+j20) JL$. Calculate the line currents and the active power of the load for the following configurations of load impedance:

a) a wye-connected system, b) a delta-connected system



$$U_{ph} = \frac{U_{lL}}{\sqrt{3}} = \frac{380}{\sqrt{3}} = 218.3831 \ V$$

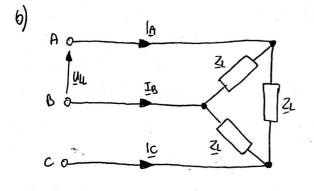
$$I_{ph} = \frac{U_{ph}}{Z_{L}} = \frac{218.3831}{30+j20} = (5.0628-j3.3753) A = 6.08 e^{-j33.7°} A$$

$$I_{A} = I_{B} = I_{c} = I_{ph} = 6.08 A$$

$$S = 3 \cdot (I_{ph} \cdot I_{ph}) = 3 \cdot 219.3831 \cdot (5.0629+j3.3753) =$$

$$= (3332.3 + j2221.5) V_{A}$$

$$P = Re \{ S \} = \overline{3332.3} \ W$$



Upn =
$$Uu = 380 \text{ V}$$

 $Iph = \frac{Uph}{2!} = \frac{380}{30+j20} = (8.9692 - j5.8462) \text{ A} = 10.5383e^{-j33,7}$
 $S = 3 \text{ Uph} \cdot Iph = 3.380 \cdot (8.9682 + j5.8462) =$
 $= 9996.9 + j 6664.6 \text{ VA}$
 $P = \text{Re } \{S\} = |9996.9 \text{ W}|$